

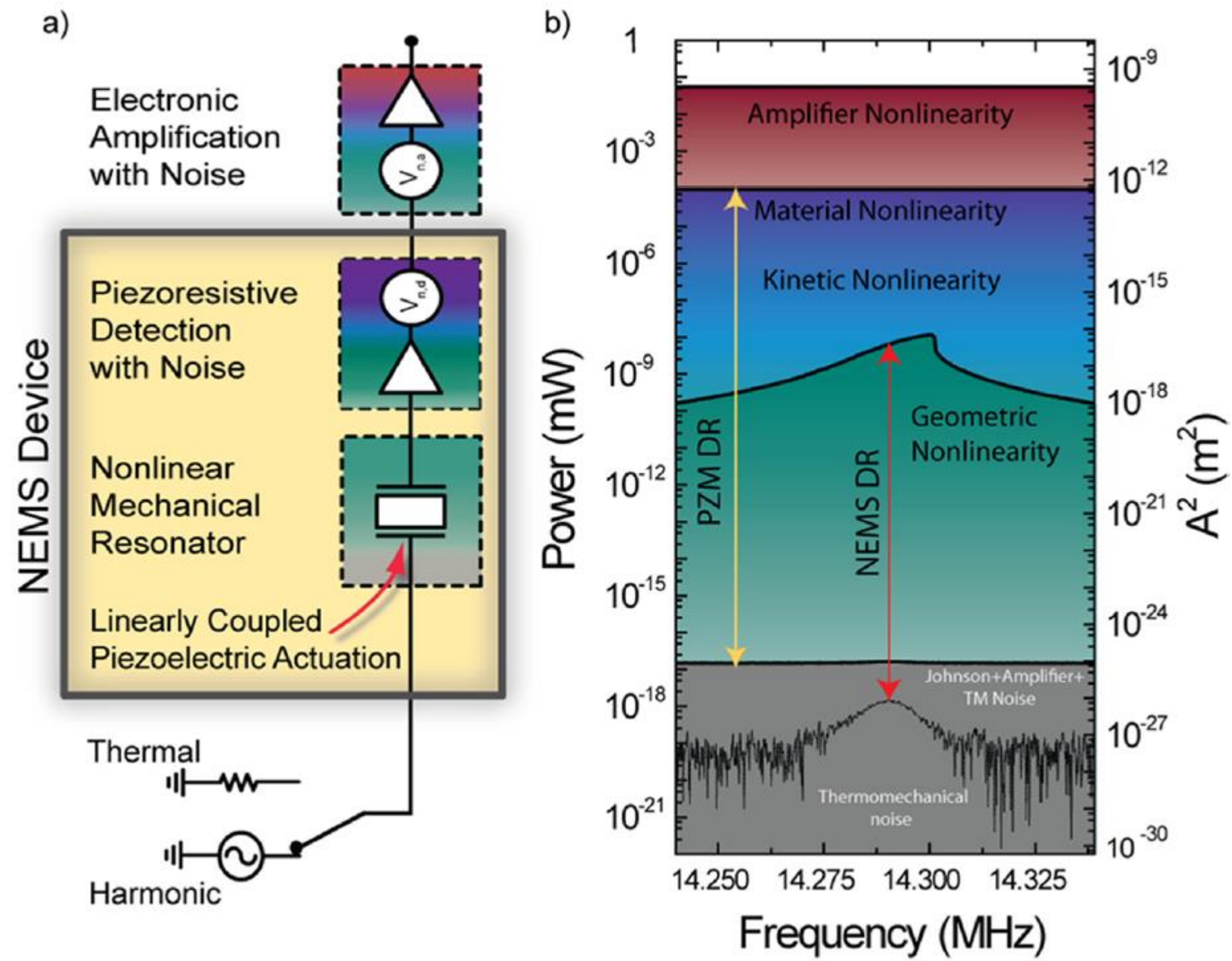
The background of the slide is a photograph of the EPFL campus in Lausanne, Switzerland. It shows modern university buildings, a large lake (Lac Léman), and distant mountains under a cloudy sky. A large red rectangle is overlaid on the right side of the image, and a blue rectangle is overlaid in the lower-middle section.

Paper 5 – Discussion

ME-426 – Micro/Nanomechanical Devices

Prof. Guillermo Villanueva

- How are the devices made?
- How is the device actuated and detected?
- Where is the nonlinearity coming from?
- Why not optical detection?
- How can Euler-Bernoulli determine the coupling constants?
- How can we separate the different noise contributions?
- Why is the signal to noise ratio larger in the inter-modal coupling?



$$\Delta\Omega_p \equiv \frac{\Delta\omega_p}{\omega_p} = \lambda_{pq} A_{\max,q}^2 \quad (2)$$

where $\Delta\Omega_p$ is the fractional frequency shift of mode p , and $A_{\max,q}$ is the maximum RMS displacement of the frequency response of mode q . Note that the Einstein summation convention is not used throughout. Calculations of the nonlinear coefficients λ_{pq} using Euler–Bernoulli theory gives (see Supporting Information)

$$\lambda_{pq} = (2 - \delta_{pq}) \frac{\tau_p}{8} \left(\frac{X_{pp} X_{qq}}{2} + X_{pq}^2 \right) \quad (3)$$

where

$$\tau_p = \frac{\eta_p}{1 + \eta_p X_{pp} \frac{TL^2}{E}}, \quad \eta_p = \frac{tw}{I \int_0^1 \Phi_p \Phi_p^{(IV)} d\xi}$$

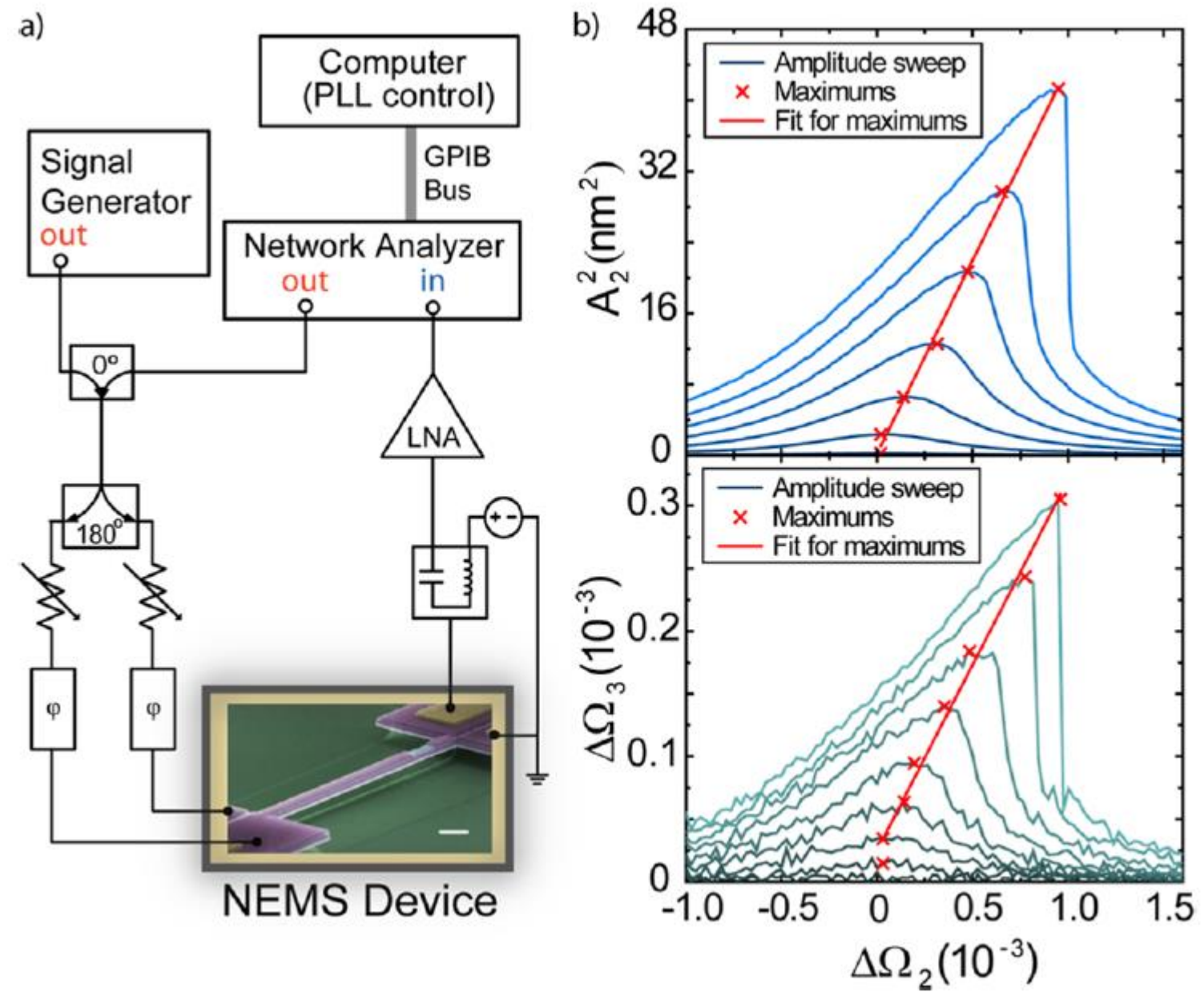


Table 1. Measured (Theoretically Calculated) Nonlinear Stiffness Coefficients λ_{pq} (10^{-5} nm^{-2}) for the First Three Out-of-Plane Flexural Modes of the Doubly-Clamped NEMS Device^a

	$q = 1$	$q = 2$	$q = 3$
$p = 1$	0.53 ± 0.01 (0.53)	1.76 ± 0.36 (1.45)	3.51 ± 0.47 (3.59)
$p = 2$	0.18 ± 0.01 (0.186)	1.16 ± 0.03 (1.16)	1.77 ± 0.13 (1.65)
$p = 3$	0.13 ± 0.01 (0.124)	0.35 ± 0.06 (0.445)	1.43 ± 0.07 (1.43)

